

2. Conservation of Energy

$$\frac{de}{dt} = - \left(\frac{P}{\rho} \right) \nabla \cdot \underline{u}$$

e: Specific internal energy
of the fluid parcel
(per unit mass!)

Total Energy is given
by

$$E = \rho \left(\frac{1}{2} \underline{u} \cdot \underline{u} + e \right)$$

Now we have $\rho \underline{u}, P, e, \rho$ 6 variables
and a system of 5 equations.

However we need to specify the equation of
state (EOS) for our fluid.

e.g.) Ideal gas: $e = \frac{P}{\rho(\gamma-1)}$

$$\gamma = \frac{f+2}{f} \quad f \text{ is the number of degrees of freedom}$$

\rightarrow Monatomic in 3D : $f=3$
in 2D : $f=2$

$$\gamma = \begin{matrix} 5/3 \\ 3D \end{matrix}, \begin{matrix} 2 \\ 2D \end{matrix}$$

$$e = \frac{k_B T}{\mu M_H}$$

mean molar mass
 $\mu = 0.5$ for a plasma
mass of hydrogen e^- , p

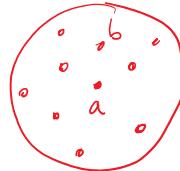
\underline{u} is the velocity of the fluid parcel
or in the SPT case the velocity of the particle. Usually we use \underline{v} for a

particle velocity, let's use \underline{v} from now on.

$$\nabla \cdot \underline{v} \stackrel{\text{red}}{=} \sum_b m_b \underline{v}_b \cdot \nabla W(|\underline{r} - \underline{r}_b|, h)$$

could use this, but better is:

$$\nabla \cdot \underline{v} = \frac{1}{\rho} [\nabla \cdot (\rho \underline{v}) - \underline{v} \cdot \nabla \rho]$$



$$\nabla \cdot \underline{v}_a \stackrel{\text{red}}{=} \frac{1}{\rho_a} \left[\sum_b m_b \frac{\rho_b \underline{v}_b}{\rho_b} \cdot \nabla_a W_{ab} - \frac{\underline{v}_a}{\rho_a} \cdot \sum_b \right]$$

$$\rho_a (\nabla \cdot \underline{v})_a = \sum_b m_b (\underline{v}_b - \underline{v}_a) \cdot \nabla_a W_{ab}$$

$\nearrow W(|\underline{r}_a - \underline{r}_b|, h)$

$$\frac{de}{dt} = - \frac{P}{\rho} \nabla \cdot \underline{v}$$

$$\boxed{\frac{de_a}{dt} = \left(\frac{\rho_a}{\rho_a^2} \right) \sum_b m_b (\underline{v}_a - \underline{v}_b) \cdot \nabla_a W_{ab}}$$

Benz
formulation

Continuity Equation : consu. of mass

$$\rho_a = \sum_b m_b W_{ab}$$

$$\underline{\text{Momentum Equation}} \quad \frac{d\underline{v}_a}{dt} = - \frac{\rho_a \nabla P_a}{\rho_a^2}$$

$$= - \frac{1}{\rho_a^2} \sum_b m_b (P_b - P_a) \nabla_a W_{ab}$$

Force $\rightarrow 0$ for const. Pressure, but linear momentum and angular momentum

are not conserved if you use this.

Instead:

$$\frac{\nabla P}{\rho} = \nabla \left(\frac{P}{\rho} \right) + \frac{P}{\rho^2} \nabla \rho$$

$$\Rightarrow \boxed{\frac{d \underline{v}_a}{dt} = - \sum_b m_b \left(\frac{P_b}{\rho_b^2} + \frac{P_a}{\rho_a^2} \right) \nabla_a w_{ab}}$$

Symmetric between $a \leftrightarrow b$
obey Newton's 3rd Law and
conserve momentum.

Add Artificial Viscosity to the SHT equations
to cause shocks (pile-ups of material)

$$\frac{d \underline{v}_a}{dt} = - \sum_b m_b \left(\frac{P_a}{\rho_a^2} + \frac{P_b}{\rho_b^2} + \Pi_{ab} \right) \nabla_a w_{ab}$$

$$\Pi_{ab} = \begin{cases} -\alpha \underline{C}_{ab} \nabla_{ab} + \beta |\nabla_{ab}|^2, & \underline{v}_{ab} \cdot \underline{\Gamma}_{ab} < 0 \\ 0, & \underline{v}_{ab} \cdot \underline{\Gamma}_{ab} > 0 \end{cases}$$

$$\nabla_{ab} = \frac{h_{ab} \underline{v}_{ab} \cdot \underline{\Gamma}_{ab}}{\underline{\Gamma}_{ab}^2 + \eta^2}$$

to avoid singularities

$$C_a = \sqrt{\frac{P_a \gamma}{\rho}}$$

$$e_a = \frac{P_a}{\rho_a(\gamma-1)}$$

$$C_a = \sqrt{\gamma(\gamma-1)e_a}$$

$$\frac{P}{\rho^2} = \frac{C^2}{\gamma \rho}$$

Variables for Particles: $\Sigma, \underline{v}, e, C, \rho$

need to calculate \underline{a} acceleration $\dot{\underline{v}}$
 \underline{v}_{pred} , e_{pred}

DRIFT1(), DRIFT2(), KICK(), CALCFORCE()

SPH:

DRIFT1($\Delta t = 0$)

CALCFORCE()

for (step = 0; step < NSTEP; ++step) {

DRIFT1($\Delta t / 2$)

CALCFORCE()

KICK(Δt)

DRIFT2($\Delta t / 2$)

}

where CALCFORCE() ≈

TREEBUILD()

NN-Density ← All particles calculate ρ

$\sqrt{\alpha(\alpha-1)} e_{\text{pred}}$ → CALCSOUND ← All particles calculate c

NN-SPHFORCE ← All calc α, \dot{e}

}

DRIFT1(Δt)

$$\underline{v} += \underline{v} \Delta t$$

$$\underline{v}_{\text{pred}} = \underline{v} + \underline{\alpha} \Delta t$$

$$e_{\text{pred}} = e + \dot{e} \Delta t$$

DRIFT2(Δt)

$$\underline{v} += \underline{v} \Delta t$$

KICK(Δt)

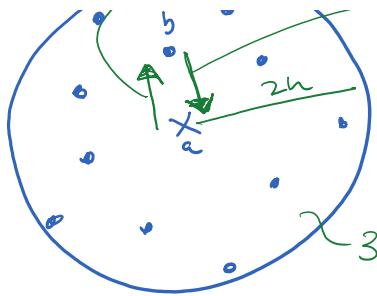
$$\underline{v} += \underline{\alpha} \Delta t$$

$$e += \dot{e} \Delta t$$

scatter operation

gather operation





32 nearest neighbors : $h_a \neq h_b$

$$W_{ab} \neq W_{ba}$$

$$W_{ab} = \frac{1}{2} (W(r_{ab}, h_a) + W(r_{ab}, h_b))$$

Symmetrize the Kernel

$$\text{or } h_{ab} = \frac{1}{2}(h_a + h_b)$$

$$\frac{dV_a}{dt} = -\frac{1}{2} \sum_b m_b \boxed{F_{ab} \nabla_a W(r_{ab}, h_a)}$$

gather part

$$-\frac{1}{2} \sum_b m_b \boxed{F_{ab} \nabla_a W(r_{ab}, h_b)}$$

rewrite a's b's

$$\frac{dV_b}{dt} = -\frac{1}{2} \sum_a m_a F_{ab} \nabla_b W(r_{ab}, h_a)$$

$$\text{but } \nabla_b = -\nabla_a$$

$$= \frac{1}{2} \sum_a m_a \boxed{F_{ab} \nabla_a W(r_{ab}, h_a)}$$

Scatter Term

So we only need to calculate the contribution $F_{ab} \nabla_a W(r_{ab}, h_a)$ once!

Typically we use 32 - 64 neighbors

Trade off between noise and resolution.

The Kernel:

$$W(r; h) = \frac{r}{h^d} \begin{cases} 6\left(\frac{r}{h}\right)^3 - 6\left(\frac{r}{h}\right)^2 + 1, & 0 \leq \frac{r}{h} < \frac{1}{2} \\ 2(1 - \left(\frac{r}{h}\right))^3, & \frac{1}{2} \leq \frac{r}{h} \leq 1 \\ 0, & \text{otherwise} \end{cases}$$

$$\tau = |\Sigma - \Sigma'| \quad \begin{cases} 0 & \text{otherwise} \\ d\text{-dimension} \end{cases}$$

$$\sigma = \begin{cases} 4/3 & \text{in 1-D} \\ 40/7\pi & \text{in 2-D} \\ 8/\pi & \text{in 3-D} \end{cases}$$

$$\frac{\partial W(\tau; h)}{\partial \tau} = \frac{6\sigma}{h^{d+1}} \begin{cases} 3\left(\frac{\tau}{h}\right)^2 - 2\left(\frac{\tau}{h}\right), & \frac{\tau}{h} < \frac{1}{2} \\ -\left(1 - \left(\frac{\tau}{h}\right)\right)^2, & \frac{1}{2} \leq \frac{\tau}{h} \leq 1 \end{cases}$$

Monaghan Kernel

\hookrightarrow Clumping instability

* Wendland Kernels are better