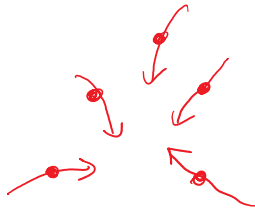




AMR

Adaptive Mesh Refinement

↳ higher resolution in the Eulerian Methods



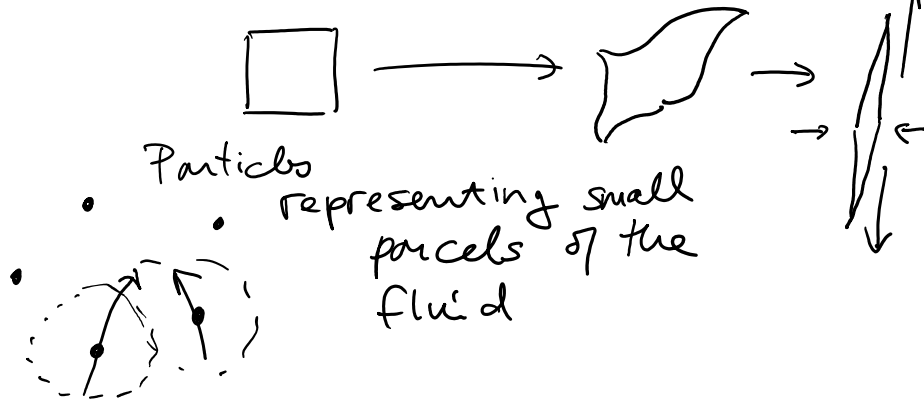
Lagrangian Methods



higher density region

2D or higher is not easy

SPH:



Particles representing small parcels of the fluid

$$\frac{d\underline{u}}{dt} \quad \text{"Time derivative follows the motion"} \equiv \frac{\underline{u}(\underline{x} + \underline{u}\delta t, t + \delta t) - \underline{u}(\underline{x}, t)}{\delta t}$$

use a Taylor expansion

$$\begin{aligned} \frac{dF}{dt} &= \frac{1}{\delta t} \left\{ F(\underline{x} + \underline{u}\delta t, t + \delta t) - F(\underline{x}, t) \right\} \\ &= \frac{1}{\delta t} \left\{ F + \frac{\partial F}{\partial x} u \delta t + \frac{\partial F}{\partial y} v \delta t + \frac{\partial F}{\partial z} w \delta t + \frac{\partial F}{\partial t} \delta t - F \right\} \end{aligned}$$

$$\underline{u} \equiv \langle u, v, w \rangle$$

$$\underline{x} \equiv \langle x, y, z \rangle$$

$$\underline{dF} = (\underline{u} \cdot \nabla) F + \frac{\partial F}{\partial t}$$

Convective derivative

$$\boxed{\frac{dF}{dt} = (\underline{u} \cdot \nabla) F + \frac{\partial F}{\partial t}}$$

Convective derivative

$$\frac{d\underline{u}}{dt} = \underline{u} \cdot \nabla \underline{u} + \frac{\partial \underline{u}}{\partial t}$$

$$m \cdot \underline{a} = \underline{F} \quad \leftarrow \begin{array}{l} \text{external force} \\ \text{small volume } \Delta v \end{array}$$

$$\rho \cdot \Delta v \frac{d\underline{u}}{dt} = \underline{F} - mg$$

$$\rho \cdot \Delta v \underline{u} \cdot \nabla \underline{u} + \rho \Delta v \frac{\partial \underline{u}}{\partial t} = \rho \Delta v g$$

$$\rho \frac{\partial \underline{u}}{\partial t} + \rho \underline{u} \cdot \nabla \underline{u} = \rho g$$

does this describe the transfer of momentum?

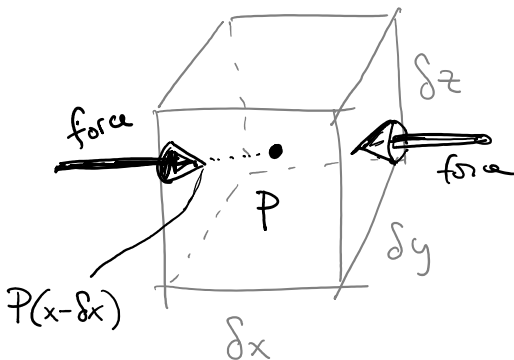
No not quite

Is this a valid equation of motion?

We are missing the pressure contribution to momentum transfer!

$$\frac{d\underline{u}}{dt} = g - \frac{\nabla P}{\rho}$$

Euler equation: 
$$\boxed{\frac{\partial \underline{u}}{\partial t} + \underline{u} \cdot \nabla \underline{u} = g - \frac{\nabla P}{\rho}}$$



$P$ , isotropic

in +ve x-direction:  $\left\{ P - \frac{1}{2} \frac{\partial P}{\partial x} \delta x \right\} \delta y \delta z$

Pressure is force per unit Area

in -ve x-direction:  $\left\{ P + \frac{1}{2} \frac{\partial P}{\partial x} \delta x \right\} \delta y \delta z$

$$= - \frac{\partial P}{\partial x} \delta x \delta y \delta z$$

this is the net force on the cube due to the pressure ... in the x-direction.

do the same for the y and z directions

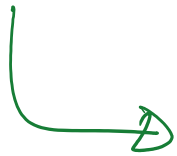
Generalize

cube due to the pressure gradient in the x-direction.

For just x we get:

$$\rho \frac{du}{dt} = \rho g_x - \frac{\partial P}{\partial x} \delta x \delta y \delta z$$

$$\frac{du}{dt} = g_x - \frac{1}{\rho} \frac{\partial P}{\partial x}$$



$$\frac{du}{dt} = g - \frac{\nabla P}{\rho}$$

$$\frac{\partial \underline{u}}{\partial t} + \underline{u} \cdot \nabla \underline{u} = g - \frac{\nabla P}{\rho}$$

SPH - use particles to follow the flow and consider the various integrals in the conservation laws and use interpolations for these.

Consider an integral interpolant

$$A_I(\underline{r}) = \int_{\text{All Space}} A(\underline{r}') W(\underline{r} - \underline{r}'; h) d\underline{r}'$$

approximate this via summation

Kernel  $\left\{ \begin{array}{l} 1^{\text{st}} \int W d\underline{r} = 1 \\ 2^{\text{nd}} \lim_{h \rightarrow 0} W(\underline{r} - \underline{r}'; h) = \delta(\underline{r} - \underline{r}') \end{array} \right.$

$$A_S(\underline{r}) = \sum_b m_b \frac{A_b}{\rho_b} W(\underline{r} - \underline{r}_b, h)$$

Also approximate its gradient

$$\nabla A_s(\mathbf{r}) = \sum_b m_b \frac{A_b}{\rho_b} \nabla W(\mathbf{r} - \mathbf{r}_b, h)$$

although higher accuracy is obtained

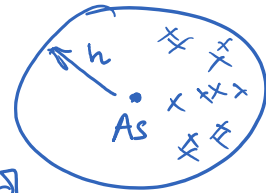
$$\rho \nabla A = \nabla(\rho A) - A \nabla \rho$$

Kernels:  $W(x, h) = \frac{1}{h\sqrt{\pi}} e^{-\left(\frac{x^2}{h^2}\right)}$

fine but we want "compact" kernel that goes over some local region.

What is the error in the approximation of  $A_{\pm}$  by  $A_s$ ? Depends a lot on how disordered the particles are good (typically)  $\mathcal{O}(h^2)$

BAD:



Ignore points outside of the kernel in the computation of  $A_s$ !

What variables do we already have  
 $\underline{u}$ ,  $P$ , and  $\rho$  5-variables  
 so we need at least 2 more equations to close the system.

Special Cases:

isothermal flow:  $P \propto \rho$  → only 1 more equation

incompressible flow:  $\rho$  is given →

What are these equations?

What are these equations.

1. Continuity Equation: conservation of mass
2. Energy Equation: exchange of energy between a fluid parcel and its environment.

Consider again the infinitesimal cube net inflow in +ve x-direction

$$\left\{ \rho u - \frac{1}{2} \frac{\partial(\rho u)}{\partial x} \delta x \right\} \delta y \delta z$$

$$\text{net inflow} \Rightarrow - \frac{\partial(\rho u)}{\partial x} \delta x \delta y \delta z$$

$$\text{Total net inflow} = -\nabla \cdot (\rho \underline{u}) \delta V$$

$$\boxed{\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{u}) = 0}$$

Continuity Equation

$$\underline{u} \cdot \nabla \rho + \rho \nabla \cdot \underline{u}$$

$$\boxed{\frac{d\rho}{dt} + \rho \nabla \cdot \underline{u} = 0}$$

Lagrangian Formulation of the Continuity equation.

For incompressible fluid this term is zero  $\rightarrow$  Derivative of  $\rho$  following the flow is also zero.